

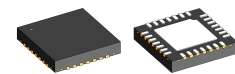
FEATURES

- ◆ 6 current-limited and short-circuit-proof push-pull drivers
- ◆ Differential 3-channel operation selectable
- ◆ Integrated impedance adaption for 30 to 140 Ω lines
- ◆ Wide power supply range from 4 to 40 V
- ◆ 200 mA output current (at VB = 24 V)
- ◆ Low output saturation voltage (< 0.4 V at 30 mA)
- ◆ Compatible with TIA/EIA standard RS-422
- ◆ Tristate switching of outputs enables use in buses
- ◆ Short switching times and high slew rates
- ◆ Low static power dissipation
- ◆ Dynamic power dissipation reduced with iC-xSwitch
- ◆ Schmitt trigger inputs with pull-down resistors, TTL and CMOS compatible; voltage-proof up to 40 V
- ◆ Thermal shutdown with hysteresis
- ◆ Error message trigger input TNER
- ◆ Open-drain error output NER, active low with excessive chip temperature and undervoltage at VCC or VB
- ◆ Operating temperature range from -40 to 125 °C

APPLICATIONS

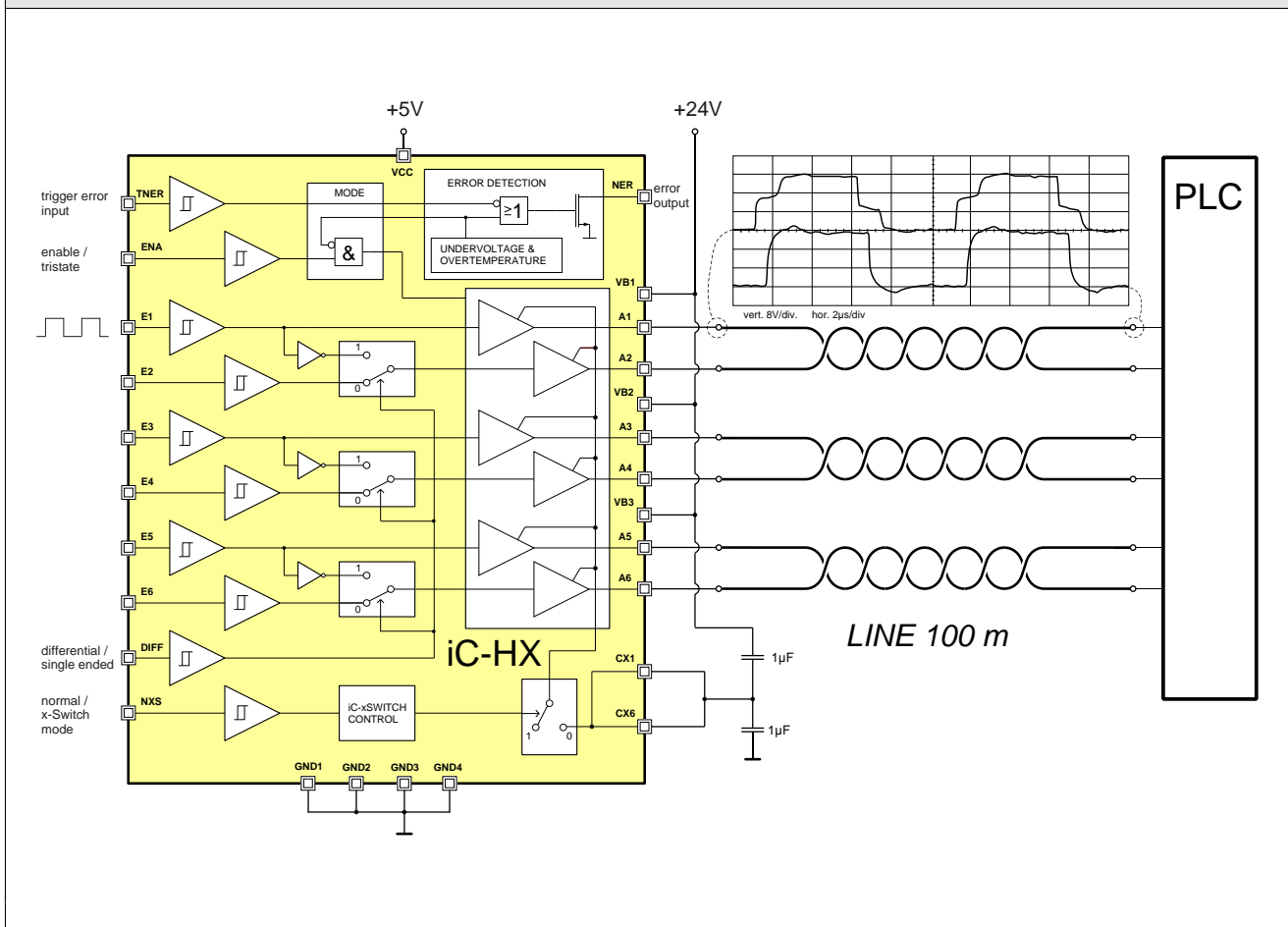
- ◆ Line drivers for 24 V control engineering
- ◆ Linear scales and encoders
- ◆ MR sensor systems

PACKAGES



QFN28 5x5 mm²

BLOCK DIAGRAM



DESCRIPTION

iC-HX is a fast line driver with six independent channels and integrated impedance adaptation for 30 to 140 Ω lines.

Channels are paired for differential 3-channel operation by a high signal at the DIFF input, providing differential output signals for the three inputs E1, E3 and E5. All inputs are compatible with CMOS and TTL levels.

The push-pull output stages have a driver power of typically 200 mA from 24 V and are short-circuit-proof and current-limited, shutting down with excessive temperature. For bus applications the output stages can be switched to high impedance using input ENA.

To reduce the dynamic power dissipation in applications with long lines the iC-HX uses the iC-xSwitch.

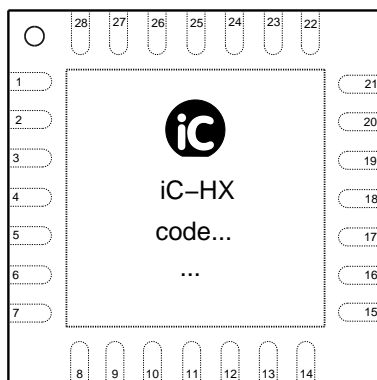
iC-HX monitors supply voltages VB and VCC and the chip temperature, switching all output stages to high impedance in the event of error and set NER active low. In addition, the device also monitors voltage differences at the pins VB1, VB2 and VB3 and generates an error signal if the absolute value exceeds 0.75 V.

The open-drain output NER allows the device to be wired-ORed to the relevant NER error outputs of other iC-HXs and iC-DLs. Via input TNER the message outputs of other ICs can be extended to generate system error messages. NER switches to high impedance if supply voltage VCC ceases to be applied.

The device is protected against ESD.

PACKAGING INFORMATION QFN28 to JEDEC Standard

PIN CONFIGURATION QFN28 5 x 5 mm²



PIN FUNCTIONS

No. Name Function

1	E1	Input Channel 1
2	E2	Input Channel 2
3	E3	Input Channel 3
4	n.c.	
5	E4	Input Channel 4

PIN FUNCTIONS

No. Name Function

6	E5	Input Channel 5
7	E6	Input Channel 6
8	VCC	+5 V Supply
9	CXS6	Capacitor iC-xSwitch
10	TNER	Error Input, low active
11	NER	Error Output, active low
12	A6	Output Channel 6
13	GND4	Ground
14	VB3	+4.5 ... 40 V Power Supply
15	A5	Output Channel 5
16	GND3	Ground
17	A4	Output Channel 4
18	VB2	+4.5 ... 40 V Power Supply
19	A3	Output Channel 3
20	GND2	Ground
21	A2	Output Channel 2
22	VB1	+4.5 ... 40 V Power Supply
23	GND1	Ground
24	A1	Output Channel 1
25	NXS	Enable iC-xSwitch, low active
26	ENA	Enable Input, high active
27	CXS1	Capacitor iC-xSwitch
28	DIFF	Differential Mode Input, high active

The pins VB1, VB2 and VB3 must be connected to the same driver supply voltage VB. The pins GND1, GND2, GND3 and GND4 must be connected to GND. To improve heat dissipation, the *thermal pad* at the bottom of the package should be joined to an extended copper area which must have GND potential.

ABSOLUTE MAXIMUM RATINGS

Beyond these values damage may occur; device operation is not guaranteed. Absolute Maximum Ratings are no Operating Conditions. Integrated circuits with system interfaces, e.g. via cable accessible pins (I/O pins, line drivers) are per principle endangered by injected interferences, which may compromise the function or durability. The robustness of the devices has to be verified by the user during system development with regards to applying standards and ensured where necessary by additional protective circuitry. By the manufacturer suggested protective circuitry is for information only and given without responsibility and has to be verified within the actual system with respect to actual interferences.

Item No.	Symbol	Parameter	Conditions	Min. Max.		Unit
				Min.	Max.	
G001	VCC	Voltage at VCC		0	7	V
G002	VBx	Voltages at VB1, VB2, VB3		0	40	V
G003	V()	Voltage at E1...6, A1...6, DIFF, ENA, TNER		0	40	V
G004	I(Ax)	Current in Ax (x=1...6)		-800	800	mA
G005	I(Ex)	Current in E1...E6, Diff, ENA, TNER		-4	4	mA
G006	V(NER)	Voltage at NER		0	40	V
G007	I(NER)	Current in NER		-4	25	mA
G008	V()	ESD Suceptibility at all pins	HBM 100 pF discharged through 1.5 k Ω		2	kV
G009	Tj	Operating Junction Temperature		-40	140	$^{\circ}$ C
G010	Ts	Storage Temperature Range		-40	150	$^{\circ}$ C

THERMAL DATA

Operating conditions: VB1...3 = 4.5...40 V, VCC = 4.5...5.5 V or VB1...3 = VCC = 4...5.5 V

Item No.	Symbol	Parameter	Conditions	Min. Typ. Max.			Unit
				Min.	Typ.	Max.	
T01	Ta	Operating Ambient Temperature Range		-40		125	$^{\circ}$ C
T02	Rthja	Thermal Resistance Chip to Ambient	surface mounted, <i>thermal pad</i> soldered to approx. 2 cm 2 heat sink		40		K/W

ELECTRICAL CHARACTERISTICS

Operating Conditions: $V_{B1...3} = 4.5...32\text{ V}$, $V_{CC} = 4...5.5\text{ V}$, $T_j = -40...140\text{ }^\circ\text{C}$, unless otherwise noted
 input level $l_o = 0...0.45\text{ V}$, $h_i = 2.4\text{ V}...V_{CC}$, timing diagram see Fig. 2

Item No.	Symbol	Parameter	Conditions				Unit
				Min.	Typ.	Max.	
General							
001	V_{Bx}	Supply Voltage Range (Driver)	for $V_{B1...3}$ voltages below 7V use setup given in Fig. 1	4		40	V
002	$I(V_{Bx})$	Supply Current in $V_{B1...3}$	$A_x = l_o$			8	mA
003	$I(V_{Bx})$	Supply Current in $V_{B1...3}$	$A_x = h_i$			8	mA
004	$I(V_{Bx})$	Supply Current in V_{B1} , Outputs $A1...2$ Tri-State	$EN_A = l_o$, $V(A1...2) = -0.3...(V_B + 0.3\text{ V})$			4	mA
005	$I(V_{Bx})$	Supply Current in $V_{B2...3}$, Outputs $A3...6$ Tri-State	$EN_A = l_o$, $V(A3...6) = -0.3...(V_B + 0.3\text{ V})$			2	mA
006	$I_O(A_x)$	Output Leakage Current	$EN_A = l_o$, $V(A_x) = 0 \dots V_B$	-50		50	μA
007	VCC	Supply Voltage Range (Logic)	for $V_{B1...3}$ voltages below 7V use setup given in Fig. 1	4		5.5	V
008	$I(V_{CC})$	Supply Current in VCC	$EN_A = h_i$, $A_x = l_o$			10	mA
009	$V_c(l_o)$	Clamp Voltage low at pins $V_{B1...3}$, $A1...6$, $E1...6$, DIFF, EN_A TNER, NER, VCC	$I() = -10\text{ mA}$, all other pins open	-1.2		-0.35	V
010	$V_c(h_i)$	Clamp Voltage high at pins $V_{B1...3}$, $A1...6$, $E1...6$, DIFF, EN_A TNER, NER	$I() = 1\text{ mA}$, all other pins open	41		64	V
011	$I(V_B)$	Supply Current in $V_{B1...3}$	$EN_A = h_i$, $f(E1...6) = 1\text{ MHz}$			50	mA
Driver Outputs $A1...6$, Low-Side-action ($x = 1...6$)							
101	$V_s(A_x)l_o$	Saturation Voltage low	$I(A_x) = 10\text{ mA}$, $A_x = l_o$			0.2	V
102	$V_s(A_x)l_o$	Saturation Voltage low	$I(A_x) = 30\text{ mA}$, $A_x = l_o$			0.4	V
103	$I_{sc}(A_x)l_o$	Short circuit current low	$V(A_x) = 1.5\text{ V}$	30	50	70	mA
104	$I_{sc}(A_x)l_o$	Short circuit current low	$V(A_x) = V_B$, $A_x = l_o$			800	mA
105	$R_{out}(A_x)$	Output resistance	$V_B = 10...40\text{ V}$, $V(A_x) = 0.5 * V_B$	40	75	100	Ohm
106	$SR(A_x)l_o$	Slew Rate low	$V_B = 40\text{ V}$, $C_l(A_x) = 100\text{ pF}$	200		1000	$\text{V}/\mu\text{s}$
107	$V_c(l_o)$	Free Wheel Clamp Voltage low	$I(A_x) = -100\text{ mA}$	-1.4		-0.5	V
Driver Outputs $A1...6$, High-Side-action ($x = 1...6$)							
201	$V_s(A_x)h_i$	Saturation Voltage high	$V_s(A_x)h_i = V_B - V(A_x)$, $I(A_x) = -10\text{ mA}$, $A_x = h_i$			0.2	V
202	$V_s(A_x)h_i$	Saturation Voltage high	$V_s(A_x)h_i = V_B - V(A_x)$, $I(A_x) = -30\text{ mA}$, $A_x = h_i$			0.5	V
203	$I_{sc}(A_x)h_i$	Short circuit current high	$V(A_x) = V_B - 1.5\text{ V}$, $A_x = h_i$	-70	-50	-30	mA
204	$I_{sc}(A_x)h_i$	Short circuit current high	$V(A_x) = 0\text{ V}$, $A_x = h_i$	-800			mA
205	$R_{out}(A_x)h_i$	Output resistance	$V_B = 10...40\text{ V}$, $V(A_x) = 0.5 * V_B$	40	75	100	Ohm
206	$SR(A_x)h_i$	Slew Rate high	$V_B = 40\text{ V}$, $C_l(A_x) = 100\text{ pF}$	200		1000	$\text{V}/\mu\text{s}$
207	$V_c(A_x)h_i$	Free Wheel Clamp Voltage high	$I(A_x) = 100\text{ mA}$, $V_B = V_{CC} = \text{GND}$	0.5		1.4	V
iC-xSwitch CXS1, CXS6, $A1...6$, $V_{B1...3}$							
301	$V_{Bxs,on}$	Turn-on threshold iC-xSwitch				12.5	V
302	$V_{Bxs,off}$	Turn-off threshold iC-xSwitch		11			V
303	$V_{Bxs,hys}$	Hysteresis		150			mV
304	$R_{on}()$	On-resistance iC-xSwitch	$V_{Bx} = 40\text{ V}$, $V(CXS_x) = 20\text{ V}$, $I(A_x) = \pm 350\text{ mA}$			7	Ohm
305	$V_{th}(A_x)h_i$	Higher threshold hi	$V_{Bx} = 12.5 \dots 40\text{ V}$			73	% V_B
306	$V_{th}(A_x)l_o$	Higher threshold lo	$V_{Bx} = 12.5 \dots 40\text{ V}$	63			% V_B
307	$V_{th}(A_x)hys$	Higher hysteresis	$V_{Bx} = 12.5 \dots 40\text{ V}$	100			mV
308	$V_{tl}(A_x)h_i$	Lower threshold hi	$V_{Bx} = 12.5 \dots 40\text{ V}$			40	% V_B
309	$V_{tl}(A_x)l_o$	Lower threshold lo	$V_{Bx} = 12.5 \dots 40\text{ V}$	30			% V_B
310	$V_{tl}(A_x)hys$	Lower hysteresis	$V_{Bx} = 12.5 \dots 40\text{ V}$	100			mV
Switch control							
401	t_{dmin}	Minimum time for line reflection	$V_B = 12.5 \dots 40\text{ V}$	100	200	300	ns
402	$t_{XSon}(A_x)$	On-time iC-xSwitch	$f(Ex) = 500\text{ KHz}$, $t_d = 800\text{ ns}$, $V_B = 12.5 \dots 40\text{ V}$	400		700	ns

ELECTRICAL CHARACTERISTICS

Operating Conditions: $V_{B1...3} = 4.5...32\text{ V}$, $V_{CC} = 4...5.5\text{ V}$, $T_j = -40...140\text{ }^\circ\text{C}$, unless otherwise noted
input level $l_o = 0...0.45\text{ V}$, $h_i = 2.4\text{ V}...V_{CC}$, timing diagram see Fig. 2

Item No.	Symbol	Parameter	Conditions	Min.	Typ.	Max.	Unit
403	tXSon(Ax)	On-time iC-xSwitch	f(Ex) = 100 KHz, $t_d = 4\text{ }\mu\text{s}$, $V_B = 12.5...40\text{ V}$	3.1		3.9	μs
CXS-generation CXS1, CXS6							
501	V()	Voltage at CXS1, CXS6	$V_B = 12.5...40\text{ V}$, $I(\text{CXSx}) = \pm 100\text{ }\mu\text{A}$	47	50	53	%VB
502	Isc()lo	Short circuit current lo	$V_B = 12.5...40\text{ V}$, $\text{CXSx} = 0\text{ V}$	2		20	mA
503	Isc()hi	Short circuit current hi	$V_B = 12.5...40\text{ V}$, $\text{CXSx} = V_B$	-20		-2	mA
504	Vc()hi	Clamp Voltage hi	$I() = 10\text{ mA}$, $V_B = V_{CC} = \text{GND}$	0.5		1.4	V
505	Vth()hi	higher turn-off threshold iC-xSwitch	$V_B = 12.5...40\text{ V}$			73	%VB
506	Vth()lo	higher turn-on threshold iC-xSwitch	$V_B = 12.5...40\text{ V}$	63			%VB
507	Vth()hys	Hysteresis	$V_{th}(\text{hys}) = V_{th}(\text{hi}) - V_{th}(\text{lo})$	100			mV
508	Vtl()hi	lower turn-on threshold iC-xSwitch	$V_B = 12.5...40\text{ V}$			40	%VB
509	Vtl()lo	lower turn-off threshold iC-xSwitch	$V_B = 12.5...40\text{ V}$	30			%VB
510	Vtl()hys	Hysteresis	$V_{tl}(\text{hys}) = V_{tl}(\text{hi}) - V_{tl}(\text{lo})$	100			mV
Inputs E1...6, DIFF, ENA, TNER							
601	Vt()hi	Threshold Voltage high				2.1	V
602	Vt()lo	Threshold Voltage low		0.8			V
603	Vt()hys	Input Hysteresis	$V_{t}(\text{hys}) = V_{t}(\text{hi}) - V_{t}(\text{lo})$	200	400	800	mV
604	Ipd()	Pull-Down-Current	$V() = 0.8\text{ V}$	10		80	μA
605	Ipd()	Pull-Down-Current	$V() \leq 40\text{ V}$	15		160	μA
606	II(E1...6)	Leakage current at E1...6	ENA = lo	-10		10	μA
Supply Voltage Control VB							
701	VBon	Threshold Value at VB for Under-voltage Detection on	$ V_{B1} - V_{B2} \ \& \ V_{B2} - V_{B3} \ \& \ V_{B1} - V_{B3} < 0.75\text{ V}$			3.95	V
702	VBoff	Threshold Value at VB for Under-voltage Detection off	$ V_{B1} - V_{B2} \ \& \ V_{B2} - V_{B3} \ \& \ V_{B1} - V_{B3} < 0.75\text{ V}$	3			V
703	VBhys	Hysteresis	$V_{Bhys} = V_{Bon} - V_{Boff}$	150			mV
Supply Voltage Difference Control VB1...3							
801	Vth(VBx)	Threshold Condition for Supply Voltage Difference Control	$\Delta V(\text{VBx}) = \text{MAX} (V_{B1} - V_{B2} , V_{B2} - V_{B3} , V_{B1} - V_{B3})$ NER \Rightarrow low	0.75		1.85	V
Supply Voltage Control VCC							
901	VCCon	Threshold Value at VCC for Under-voltage Detection on				3.95	V
902	VCCoff	Threshold Value at VCC for Under-voltage Detection off		3			V
903	VCChys	Hysteresis	$V_{CChys} = V_{CCon} - V_{CCoff}$	100			mV
Temperatur Control							
A01	Toff	Thermal Shutdown Threshold	increasing temperature	145		175	$^\circ\text{C}$
A02	Ton	Thermal Lock-on Threshold	decreasing temperature	130		165	$^\circ\text{C}$
A03	Thys	Thermal Shutdown Hysteresis	$\text{Thys} = T_{on} - T_{off}$	4	12		$^\circ\text{C}$
Error Output NER							
B01	Vs()	Saturation Voltage low at NER	$I(\text{NER}) = 5\text{ mA}$, $\text{NER} = l_o$			0.6	V
B02	Isc()	Short Circuit Current low at NER	$V(\text{NER}) = 2...40\text{ V}$, $\text{NER} = l_o$	6	12	20	mA
B03	IO()	Leakage Current at NER	$V(\text{NER}) = 0\text{ V}...V_B$, $\text{NER} = h_i$	-10		10	μA
B04	VCC	Supply Voltage for NER function	$I(\text{NER}) = 5\text{ mA}$, $\text{NER} = l_o$, $V_s(\text{NER}) < 0.6\text{ V}$	2.9			V

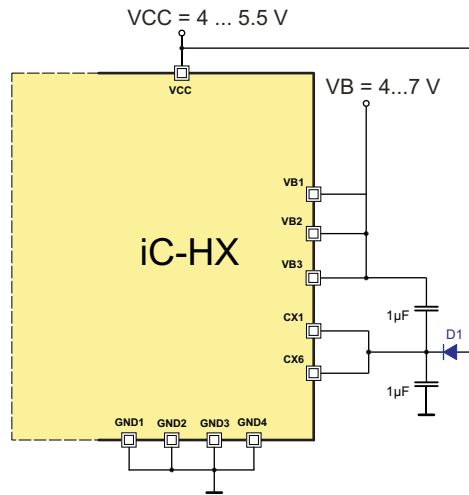


Figure 1: Operating setup for VBx voltages below 7V using additional diode D1 (1N4148 or equivalent)

OPERATING REQUIREMENTS

Operating Conditions: VB1...3 = 4.5...32 V, VCC = 4...5.5 V, Tj = -40...140 °C, unless otherwise noted
input level lo = 0...0.45 V, hi = 2.4 V...VCC, timing diagram see fig. 2

Item No.	Symbol	Parameter	Conditions	Min.		Unit
					Max.	
Time Delays						
I001	t _{plh} (E-A)	Propagation Delay Ex ⇒ Ax	DIFF = lo, Cl() = 100 pF		400	ns
I002	t _{phl} (E-A)	Propagation Delay Ex ⇒ Ax	DIFF = lo, Cl() = 100 pF		200	ns
I003	Δt _{plh} (Ax)	Propagation Delay Skew A1 ⇒ A2 , A3 ⇒ A4 , A5 ⇒ A6	DIFF = hi, Cl() = 100 pF		100	ns
I004	Δt _{phl} (Ax)	Propagation Delay Skew A1 ⇒ A2 , A3 ⇒ A4 , A5 ⇒ A6	DIFF = hi, Cl() = 100 pF		100	ns
I005	t _{plh} (ENA)	Propagation Delay ENA ⇒ Ax	Ex = hi, DIFF = lo, Cl() = 100 pF, RI(Ax, GND) = 5 kΩ		300	ns
I006	t _{phl} (ENA)	Propagation Delay ENA ⇒ Ax	Ex = lo, DIFF = lo, Cl() = 100 pF, RI(VB, Ax) = 100 kΩ		200	ns
I007	t _{plh} (ENA)	Propagation Delay ENA ⇒ Ax	Ex = lo, DIFF = lo, RI(VB, Ax) = 5 kΩ		500	ns
I008	t _{phl} (ENA)	Propagation Delay ENA ⇒ Ax	Ex = hi, DIFF = lo, RI(Ax, GND) = 5 kΩ		500	ns
I009	t _{plh} (DIFF)	Propagation Delay DIFF ⇒ A2, A4, A6	E1, E3, E5 = hi, Cl() = 100 pF		250	ns
I010	t _{phl} (DIFF)	Propagation Delay DIFF ⇒ A2, A4, A6	E1, E3, E5 = lo, Cl() = 100 pF		400	ns
I011	t _{plh} (TNER)	Propagation Delay TNER ⇒ NER	RI(VB, NER) = 5 kΩ, Cl() = 100 pF		2	μs
I012	t _{po} ff(VBx)	Turn-off delay, VBx ⇒ NER	VBx - VB _y > V _{th} (VBx), x <> y, x, y = 1..3	0.3	3	μs

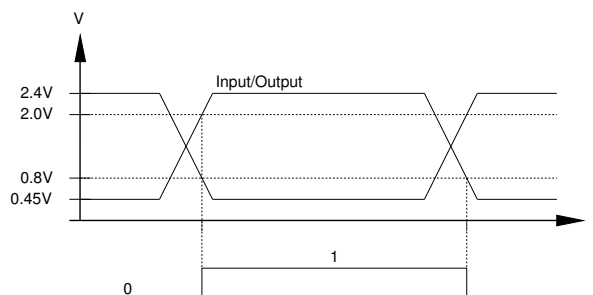


Figure 2: Reference levels for delays

DESCRIPTION

Line drivers for control engineering couple TTL- or CMOS-compatible digital signals with 24 V systems via cables. The maximum permissible signal frequency is dependent on the capacitive load of the outputs (cable length) or, more specifically, the power dissipation in iC-HX resulting from this. To avoid possible short circuiting the drivers are current-limited and shutdown with excessive temperature.

When the output is open the maximum output voltage corresponds to supply voltage V_B (with the exception of any saturation voltages). Figure 3 gives the typical DC output characteristic of a driver as a function of the load. The differential output resistance is typically 75Ω over a wide voltage range.

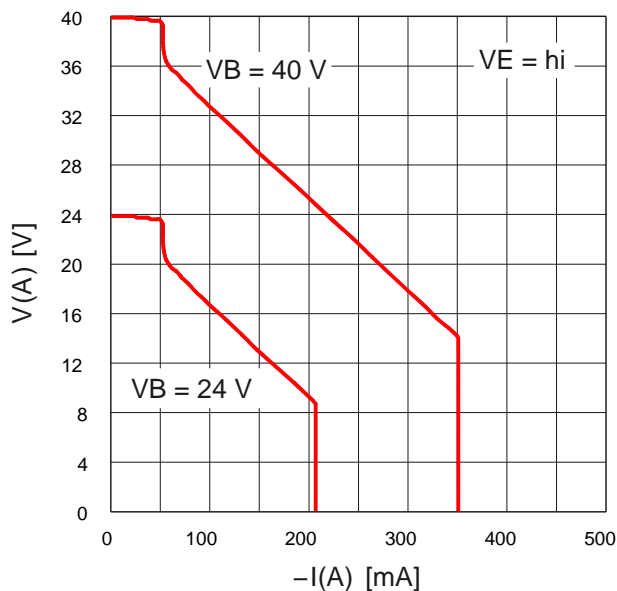


Figure 3: Load dependence of the output voltage (High-side stage)

Each open-circuited input is set to low by an internal pull-down current source; an additional connection to GND increases the device's immunity to interference. The inputs are TTL- and CMOS-compatible. Due to their high input voltage range, the inputs can also be set to high-level by applying VCC or V_B .

LINE EFFECTS

In PLC systems data transmission using 24 V signals usually occurs without a matched line termination. A mismatched line termination generates reflections which travel back and forth if there is also no line adaptation on the driver side of the device. With rapid pulse trains transmission is disrupted. In iC-HX, however, fur-

ther reflection of back travelling signals is prevented by an integrated impedance network, as shown in Figure 4.

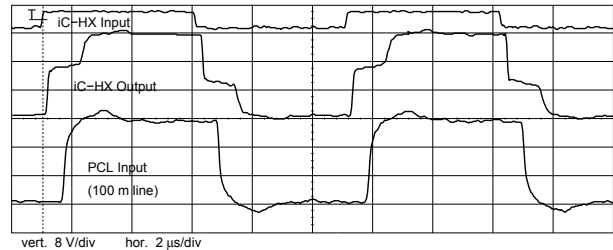


Figure 4: Reflections caused by a mismatched line termination

During a pulse transmission the amplitude at the iC-output initially only increases to half the value of supply voltage V_B as the internal driver resistance and characteristic line impedance form a voltage divider. A wave with this amplitude is coupled into the line and experiences after a delay a total reflection at the high-impedance end of the line. At this position, the reflected wave superimposes with the transmitted wave and generates a signal with the double wave amplitude at the receiving device.

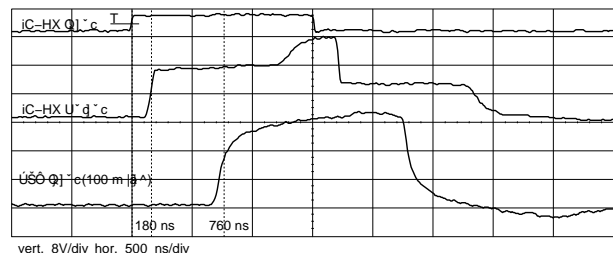


Figure 5: Pulse transmission and transit times

After a further delay, the reflected wave also increases the driver output to the full voltage swing. iC-HX's integrated impedance adapter prevents any further reflection and the achieved voltage is maintained along and at the termination of the line.

A mismatch between iC-HX and the transmission line influences the level of the signal wave first coupled into the line, resulting in reflections at the beginning of the line. The output signal may then have a number of graduations. Voltage peaks beyond V_B or below GND are capped by integrated diodes. By this way, transmission lines with a characteristic impedance of between 30 and 140Ω thus permit correct operation of the device.

iC-xSwitch

Power dissipation in the driver occurs with each switch-

ing edge when over the double signal run time the internal resistor forms a voltage divider with the characteristic line impedance and is proportional to the length of the connected line and the switching frequency. If the internal resistor is perfectly matched to the characteristic line impedance, the voltage divider generates half the supply voltage at the line input, only supplying the full voltage when an echo occurs. iC-HX exploits this behavior of the open line in order to reduce the power dissipation in the driver. A switch is triggered by applying the halved low-impedance supply voltage, buffered with capacitors, to the line input and terminated by applying the internal resistor shortly before the echo occurs. Power dissipation occurs regardless of the length of the connected line in the time between the application of the resistor to the line and the beginning of the echo. In order to control this process iC-HX must recognize the length of the connected line. The line is measured using an integrated procedure which evaluates the line echo. This principle of power dissipation reduction only functions when a single wave travels along the line. The maximum transmission frequency with a reduced power dissipation is directly proportional to the line length. If the transmission frequency is too high for the line length, iC-xSwitch is no longer used, resulting in increased power dissipation in the driver. The required halved supply voltage is generated internally in the chip and must be buffered by capacitors. On a rising edge current flows from the capacitor into the line and back into the capacitor on a falling edge. With the differential operation of two lines the currents flow from one line to the other and back again.

Figure 6 shows the three switches, the integrated resistor to match the characteristic line impedance and the connected line. VB is the positive power supply and VB/2 is the half of it. The control of the switches depends on the input signals of the device and the length of the connected line. With all enable-signals at lo-level the output A is high impedance (tristate).

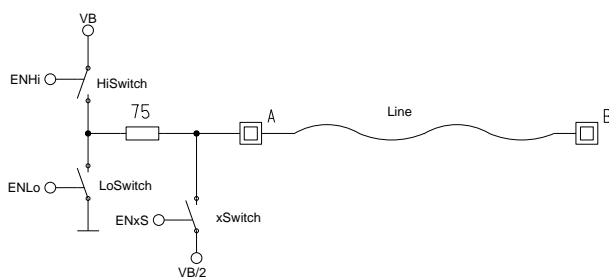


Figure 6: Circuit diagram with switches and line

Figures 7 and 8 show the input signal V(E), the switch trigger signals derived from this and the voltage curve at the beginning (A) and end (B) of the line at intervals t1 to t8. Figure 7 shows operation without iC-xSwitch. Power

dissipation $P_D(HX)$ occurs at intervals t1 to t4 and t5 to t8. Figure 8 describes operation with iC-xSwitch; power dissipation $P_D(HX)$ occurs between t3 and t4 and t7 and t8. The mean power dissipation is significant for the warming of the device, which is proportional to the duty cycle. This results in a reduced power dissipation (at the same frequency), meaning there is less power dissipation with a shorter line or through the use of iC-xSwitch with a long line, for example.

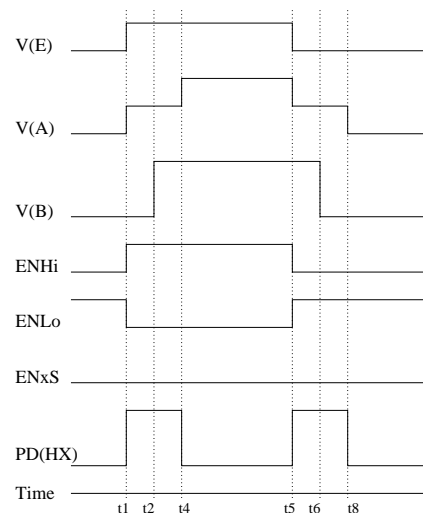


Figure 7: Power dissipation $P_D(HX)$ without iC-xSwitch

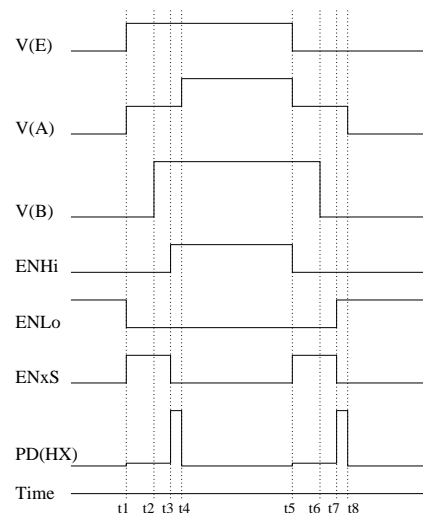


Figure 8: Power dissipation $P_D(HX)$ with iC-xSwitch

An example for the power dissipation is given in figure 9. When xSwitch is not used by setting NXS to high, the iC-HX behaves like the iC-DL.

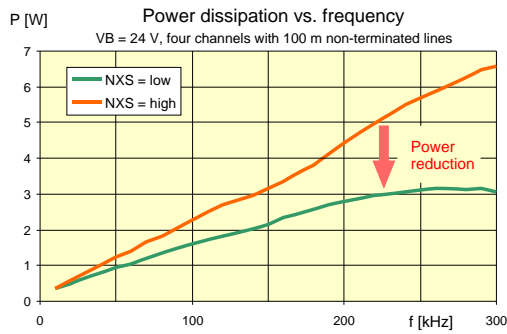


Figure 9: Power dissipation with and without xSwitch-Mode

DEMO BOARD

iC-HX is in a QFN28 package and comes with a demo board for test purposes. Figures 10 to 11 shows the wiring and the top of the demo board.

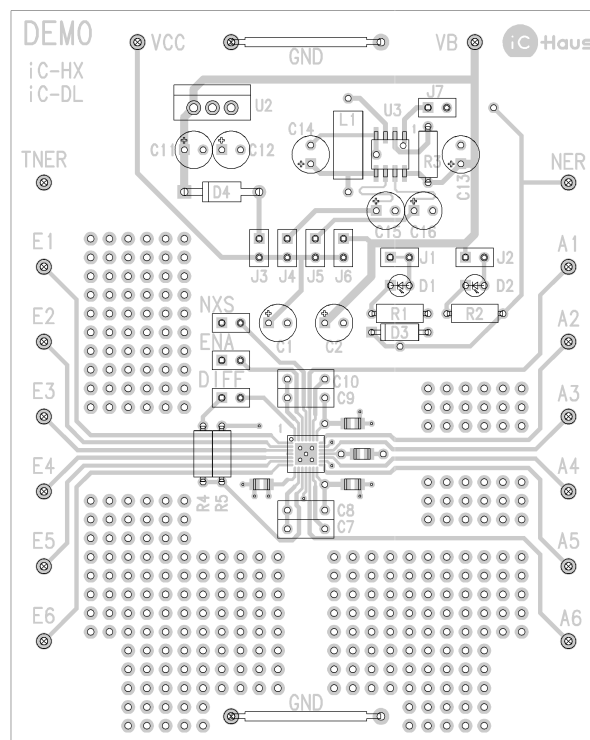


Figure 10: Demo-Board ,top view

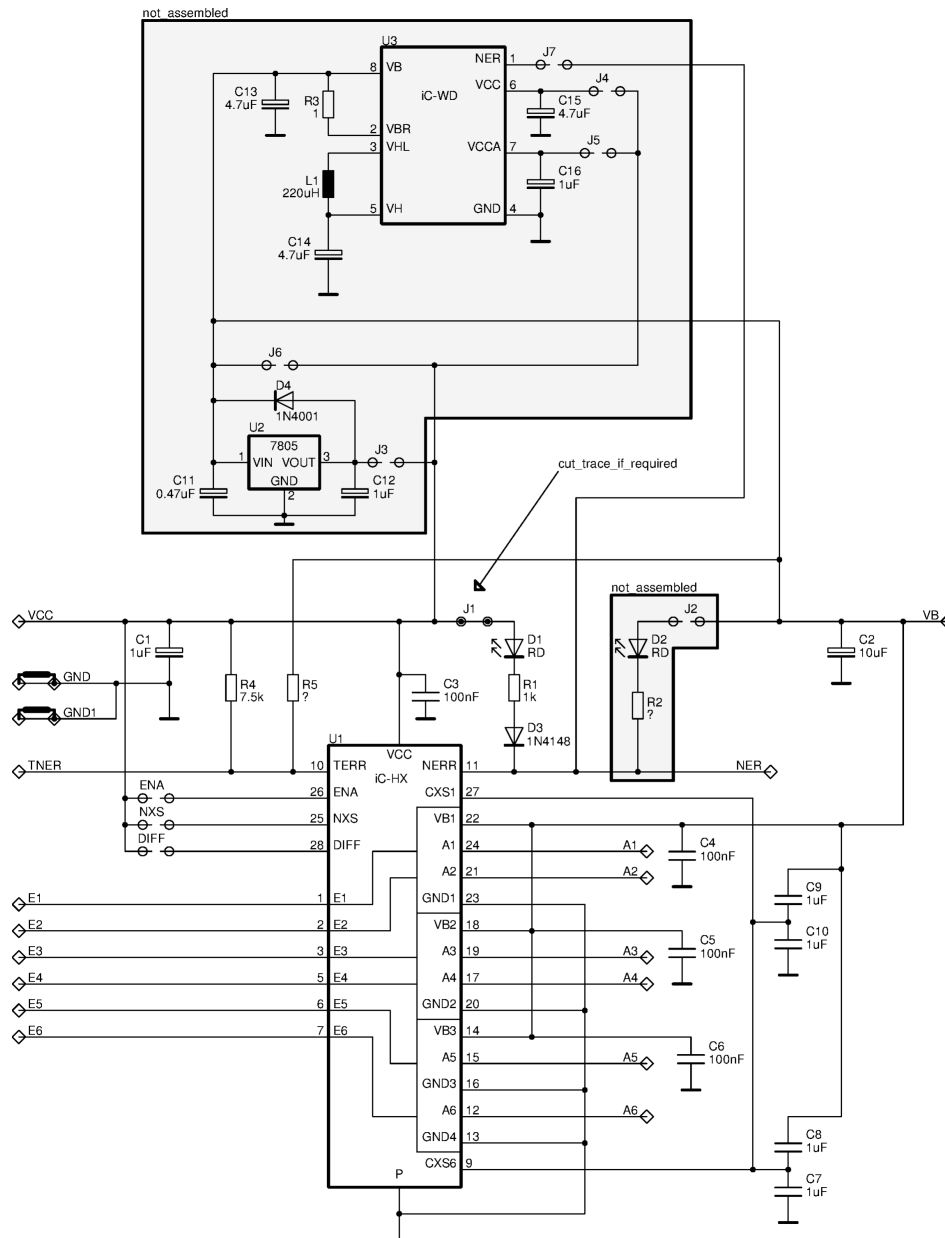


Figure 11: Circuit diagram of the demo board

REVISION HISTORY

Rel.	Rel. Date*	Chapter	Modification	Page
B2	2016-07-28		Label "preliminary" removed	1
		ELECTRICAL CHARACTERISTICS	Items 001, 007: Conditions for operation at VBx voltages below 7V introduced	4
		ELECTRICAL CHARACTERISTICS	Figure 1 introduced showing operating setup for VBx voltages below 7 V	6
		OPERATING CONDITIONS	Item I012: Parameter and condition added	6

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* Release Date format: YYYY-MM-DD

ORDERING INFORMATION

Type	Package	Order Designation
iC-HX iC-HX Evaluation Board	QFN28 5 x 5 mm ²	iC-HX QFN28 iC-HX EVAL HX2D

Please send your purchase orders to our order handling team:

Fax: +49 (0) 61 35 - 92 92 - 692

E-Mail: dispo@ichaus.com

For technical support, information about prices and terms of delivery please contact:

iC-Haus GmbH
Am Kuemmerling 18
D-55294 Bodenheim
GERMANY

Tel.: +49 (0) 61 35 - 92 92 - 0
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